

# Kinetic Studies of Ammonia Oxidation in Shock Waves. IV. Comparison of Induction Periods for the Ignition of NH<sub>3</sub>-O<sub>2</sub>-N<sub>2</sub> with Those for NH<sub>3</sub>-O<sub>2</sub>-Ar Mixtures

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Induction periods for ammonia oxidation in the NH<sub>3</sub>-O<sub>2</sub>-Ar and NH<sub>3</sub>-O<sub>2</sub>-N<sub>2</sub> mixtures were measured by monitoring an ultraviolet absorption of ammonia in reflected shock waves. For the NH<sub>3</sub>-O<sub>2</sub>-Ar mixtures, induction periods in the temperature range of 1450—2730°K were found to be expressed by

$$\log \tau_i[\text{O}_2] (\text{mol} \cdot \text{l}^{-1} \cdot \mu\text{sec}) = -(16.24 \pm 0.17) + (10080 \pm 320)/T$$

when oxygen content is in the range of 4—10%, and by

$$\log \tau_i(\mu\text{sec}) = -(2.55 \pm 0.14) + (8810 \pm 220)/T$$

when the oxygen content is less than 1%. Values of induction periods for the 0.5% NH<sub>3</sub>-0.5% O<sub>2</sub>-99% N<sub>2</sub> and 1% NH<sub>3</sub>-1% O<sub>2</sub>-98% N<sub>2</sub> mixtures were also measured and compared with those for the NH<sub>3</sub>-O<sub>2</sub> mixtures highly diluted with argon. Both results agreed well by taking into account vibrational relaxation of the reacting system if appropriate values of vibrational relaxation times for N<sub>2</sub> dilute in NH<sub>3</sub> is assumed. Therefore, possibility of coupling of vibrational relaxation of N<sub>2</sub> and oxidation reaction was considered to be small.

In the first paper of this series<sup>1,2)</sup> we found a linear relationship between  $\log \tau_i[\text{O}_2]$  and  $1/T$  for the shock-heated NH<sub>3</sub>-O<sub>2</sub>-Ar mixtures where  $\tau_i$  was induction period determined by the reaction between NH<sub>3</sub> and O<sub>2</sub>. Thereafter, we<sup>3)</sup> measured induction periods for the mixtures of 90% N<sub>2</sub>-6% NH<sub>3</sub>-4% O<sub>2</sub> and 90% N<sub>2</sub>-4% NH<sub>3</sub>-6% O<sub>2</sub>, and made Arrhenius plots by assuming two possible cases; (a) nitrogen is relaxed translationally, rotationally and vibrationally, and (b) nitrogen is relaxed translationally and rotationally. Comparison of these plots with a plot for the NH<sub>3</sub>-O<sub>2</sub>-Ar mixtures showed that data calculated for the case (b) are very close to the plot for the NH<sub>3</sub>-O<sub>2</sub>-Ar mixtures at higher temperatures but those for the case (a) approach to the latter plot at lower temperatures. This phenomenon was attributed to the effect of vibrational relaxation of nitrogen which became comparable to the induction period of ammonia oxidation in certain temperature range. Also, it was considered that the co-existence of NH<sub>3</sub> and O<sub>2</sub> might shorten the vibrational relaxation time of N<sub>2</sub>.

In order to minimize the effect of these additives and to examine the effect of vibra-

tional relaxation of N<sub>2</sub> on the oxidation reaction, measurement of induction periods was performed for the NH<sub>3</sub>-O<sub>2</sub> mixtures highly diluted with nitrogen and compared with those for the NH<sub>3</sub>-O<sub>2</sub> mixtures highly diluted with argon.

## Experimental

The experimental details have been described previously.<sup>1-4)</sup> Induction periods were measured in reflected shock waves by monitoring the absorption of NH<sub>3</sub> at 2245 Å, 2300 Å or 2400 Å. One of these wavelengths was chosen depending on the NH<sub>3</sub> concentration because the extinction coefficient of NH<sub>3</sub> was higher at shorter wavelength. The mixtures used and experimental conditions were summarized in Table 1, where data for the mixtures VIII and X were taken from the previous report.<sup>1)</sup>

## Results and Discussion

**The Induction Periods for NH<sub>3</sub>-O<sub>2</sub>-Ar Mixtures.** Arrhenius plots of  $\tau_i[\text{O}_2]$  for the mixtures I—XI are shown in Fig. 1. Here, data for the mixtures containing more than 4% oxygen are expressed by a straight line, a least-squares expressions of which is as follows:

$$\log \tau_i[\text{O}_2] (\text{mol} \cdot \text{l}^{-1} \cdot \mu\text{sec}) = -(16.24 \pm 0.17) + (10080 \pm 320)/T \quad (1)$$

This indicates that the linear relation between

1) T. Takeyama and H. Miyama, *This Bulletin*, **39**, 2352 (1966).

2) T. Takeyama and H. Miyama, *ibid.*, **39**, 2609 (1966).

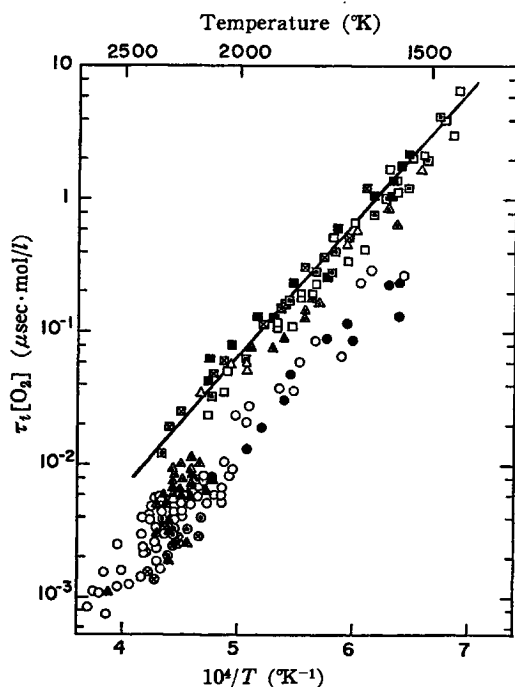
3) H. Miyama and R. Endoh, *J. Chem. Phys.*, **46**, 2011 (1967).

4) T. Takeyama and H. Miyama, *J. Chem. Phys.*, **42**, 3737 (1965); *This Bulletin*, **38**, 1670 (1965).

TABLE 1. EXPERIMENTAL CONDITIONS

Reaction mixture	Composition (%)				$T_s$ (°K)	$P_s$ (atm)	$[O_2]$ ( $10^{-3}$ mol/l)	$\tau_i$ ( $\mu$ sec)
	NH <sub>3</sub> %	O <sub>2</sub> %	Ar%	N <sub>2</sub> %				
I	0.5	0.5	99	0	1560–2230	2.61–7.41	0.0851–0.264	50–1250 (NH <sub>3</sub> 2245 Å)
II	1	0.5	98.5	0	2160–2370	3.63–3.92	0.094–0.111	16–37 (NH <sub>3</sub> 2245 Å)
III	0.5	1	98.5	0	2140–2320	3.64–3.97	0.196–0.220	11–38 (NH <sub>3</sub> 2245 Å)
IV	1	1	98	0	1560–2730	1.89–7.48	0.113–0.555	4–1230 (NH <sub>3</sub> 2245 Å)
V	2	1	97	0	2100–2580	3.41–4.05	0.161–0.229	7–36 (NH <sub>3</sub> 2245 Å)
VI	2	2	96	0	1580–2320	1.98–7.75	0.222–1.12	13–950 (NH <sub>3</sub> 2245 Å or 2300 Å)
VII	3	3	94	0	1530–2130	4.74–8.33	0.814–1.84	50–1280 (NH <sub>3</sub> 2400 Å)
VIII	6	4	90	0	1600–2300	3.49–4.51	0.741–1.32	28–1360 (OH 3067 Å)
IX	5	5	90	0	1490–2320	3.73–7.66	0.980–2.81	12–1850 (NH <sub>3</sub> 2400 Å)
X	4	6	90	0	1550–2110	3.54–5.52	1.23–2.47	37–1026 (OH 3067 Å)
XI	10	10	80	0	1450–2120	3.62–7.31	2.08–6.06	12–1400 (NH <sub>3</sub> 2400 Å)
XII	0.5	0.5	0	99	1530–2190 (1670–2490)	1.52–4.75 (1.47–4.66)	0.0504–0.184 (0.0439–0.165)	17–1580 (NH <sub>3</sub> 2245 Å)
XIII	1	1	0	98	1530–2300 (1660–2600)	1.49–4.55 (1.45–4.47)	0.0956–0.364 (0.0804–0.328)	6–1600 (NH <sub>3</sub> 2245 Å)

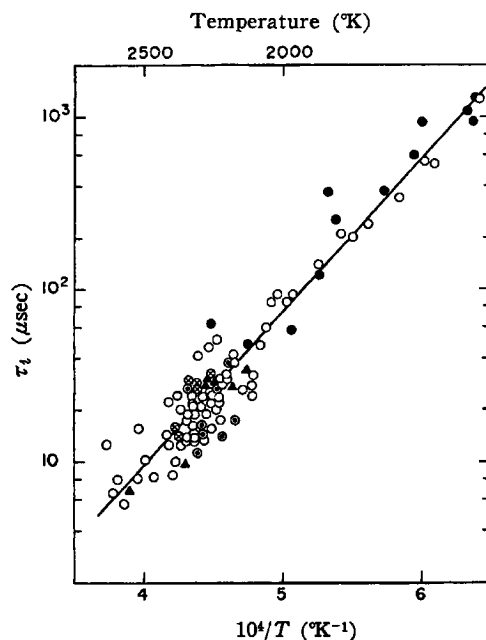
Note: Shock parameters calculated for mixtures XII and XIII correspond to case (a), and those corresponding to case (b) are shown in parentheses.  $T_s$  and  $P_s$  are temperature and pressure behind reflected shock waves.

Fig. 1. Arrhenius plot for  $\tau_i[O_2]$ .

Marks ●, ⊗, ⊙, ○, ▲, △, ▴, ▫, □, ■, and ◻ refer to mixtures I, II, III, IV, V, VI, VII, VIII, IX, X, and XI respectively.

$\log \tau_i[O_2]$  and  $1/T$  obtained previously<sup>1)</sup> holds over a wide range of oxygen concentration (4–10%).

However, when the oxygen content is less

Fig. 2. Arrhenius plot for  $\tau_i$ .

Marks are the same as in Fig. 1.

than 3%,  $\log \tau_i[O_2]$  decreases as the former decreases. Especially, when the oxygen content is less than 1%, the result is well expressed by a linear plot of  $\log \tau_i$  via  $1/T$  as shown in Fig. 2, where the solid line obtained by a least-squares calculation is expressed by:

$$\log \tau_i (\mu\text{sec}) = -(2.55 \pm 0.14) + (8810 \pm 220)/T \quad (2)$$

In order to explain this relationship from the viewpoint of chemical kinetics, available experimental data are not enough.

**The Induction Periods for  $\text{NH}_3\text{-O}_2\text{-N}_2$  Mixtures and Vibrational Relaxation of Nitrogen.** According to the preliminary experiment, the dependence of  $\tau_i$  on the oxygen content observed for  $\text{NH}_3\text{-O}_2\text{-N}_2$  was similar in tendency to that for  $\text{NH}_3\text{-O}_2\text{-Ar}$ . In order to examine the effect of vibrational relaxation of nitrogen, it is desirable to use mixtures of small ammonia and oxygen contents. There-

cases, it was assumed that the internal degrees of freedom of ammonia and oxygen are completely relaxed. From the figure, it is obvious that data calculated for the case (b) agree with the plot for the  $\text{NH}_3\text{-O}_2\text{-Ar}$  mixtures at higher temperatures and those for the case (a) at lower temperatures.

Vibrational relaxation time of nitrogen,  $\tau_{\text{N}_2\text{-N}_2}$ , is given by the expression of Milliken and White<sup>5)</sup> as follows.

$$\log P\tau_{\text{N}_2\text{-N}_2} (\text{atm} \cdot \text{sec}) = 102T^{-1/3} - 11.24 \quad (3)$$

Values of  $\tau_{\text{N}_2\text{-N}_2}$  calculated by substituting  $P=3.0$  atm, which is an average of pressures behind reflected shock waves for the mixtures XII and XIII, are also shown in Fig. 3 by a broken line. From the figure, it is seen that  $\tau_{\text{N}_2\text{-N}_2}$  is equal to  $\tau_i$  for the  $\text{NH}_3\text{-O}_2\text{-Ar}$  mixtures at 1570°K, and that  $\tau_{\text{N}_2\text{-N}_2} < \tau_i$  below this temperature and  $\tau_{\text{N}_2\text{-N}_2} > \tau_i$  above it. Therefore, it is expected that the case (a) is applicable at lower temperatures and (b) at higher temperatures. However, the crossover temperature from (a) to (b) in Fig. 3 is higher than that expected. This is considered to be due to the effect of  $\text{NH}_3$  and  $\text{O}_2$  in shortening the vibrational relaxation time.<sup>6)</sup>

It is well known<sup>6)</sup> that translational temperature of polyatomic gas behind the shock wave decreases exponentially with time  $t$  as follows.

$$\frac{T - T_a}{T_b - T_a} = \exp\left(-\frac{C_p t}{C_p' \tau_v}\right) \quad (4)$$

Here,  $T_a$  and  $T_b$  are shock wave temperatures corresponding to the cases (a) and (b),  $C_p$  is average specific heat at constant pressure,  $C_p'$  is  $C_p$  minus vibrational contribution, and  $\tau_v$  is vibrational relaxation time. For the system diluted with argon, the temperature behind shock front is almost constant during the induction period. However, for the system diluted with nitrogen, the temperature decreases from  $T_b$  and approaches to  $T_a$  during the induction period according to Eq. (4). Therefore, instead of constant temperature in the case of argon dilution, average temperature must be adopted to define temperature of the system diluted with nitrogen. Thus, temperature  $T$  of the reaction system during the induction period  $\tau_i$  is given as follows by using Eq. (4).

$$T = \frac{1}{\tau_i} \int_0^{\tau_i} T dt$$

5) R. C. Millikan and D. R. White, *J. Chem. Phys.*, **39**, 98 (1963).

6) T. L. Cottrell and J. C. McCoubrey, "Molecular Energy Transfer in Gases," Butterworths, London (1961), p. 54.

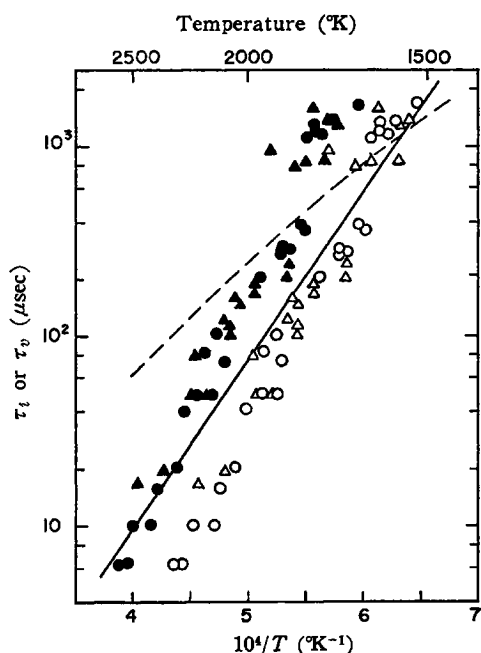


Fig. 3. Arrhenius plot for  $\tau_i$  and  $\tau_{\text{N}_2\text{-N}_2}$ .

Triangles and circles refer to mixtures XII and XIII, respectively, open marks correspond to case (a) and closed marks to case (b), and a solid and a broken line were calculated from Eqs. (2) and (3).

fore, detailed measurements were performed for the mixtures XII and XIII. The results are shown in Fig. 3, where a solid line is calculated by Eq. (2) and open and closed marks correspond to cases (a) and (b), respectively. These two cases were assumed to calculate reflected shock temperatures and oxygen concentrations from the initial pressures and incident shock velocities. As described previously,<sup>4)</sup> nitrogen is considered to be relaxed translationally, rotationally, and vibrationally for (a), and to be relaxed translationally and rotationally for (b). In both

$$= \frac{\tau_v}{\tau_i} \cdot \frac{C_p'}{C_p} (T_b - T_a) \left\{ 1 - \exp \left( - \frac{C_p' \tau_i}{C_p \tau_v} \right) \right\} \quad (5)$$

Therefore, if  $\tau_v$  is known, it is possible to

TABLE 2. PARAMETERS USED FOR THE CALCULATION OF TEMPERATURES OF THE REACTION SYSTEM

Reaction mixture	$T_a$ (°K)	$T_b$ (°K)	$P$ (atm)	$C_p/C_p'$	$\tau_i$ ( $\mu$ sec)	$T$ (°K)
XII	1550	1700	3.68	1.20	1320	1562
	1570	1720	4.71	1.20	1300	1579
	1590	1750	3.61	1.20	850	1608
	1640	1800	1.32	1.21	1580	1657
	1660	1830	4.66	1.21	800	1674
	1680	1860	3.13	1.22	790	1700
	1710	1890	3.57	1.22	240	1761
	1710	1890	1.93	1.22	210	1775
	1730	1920	1.78	1.22	970	1758
	1780	1980	2.86	1.22	170	1858
	1780	1980	3.50	1.22	190	1842
	1840	2050	1.50	1.22	160	1956
	1840	2050	2.75	1.23	105	1945
	1840	2050	4.30	1.23	110	1917
	1840	2050	3.31	1.23	170	1968
	1860	2080	3.15	1.23	130	1947
	1920	2160	2.65	1.23	50	2078
	1950	2190	3.07	1.23	50	2097
	1980	2230	2.51	1.24	80	2051
	2080	2350	2.41	1.25	20	2298
	2190	2490	2.29	1.25	17	2434
XIII	1550	1690	3.68	1.20	1600	1555
	1590	1740	3.61	1.20	1350	1596
	1610	1760	3.50	1.20	1200	1616
	1630	1790	1.62	1.21	1400	1642
	1630	1790	3.33	1.21	1250	1637
	1650	1820	3.11	1.21	1140	1658
	1650	1820	3.89	1.21	350	1670
	1680	1840	3.71	1.21	380	1698
	1700	1870	4.90	1.21	270	1719
	1730	1900	3.04	1.21	280	1758
	1730	1900	4.73	1.21	270	1749
	1780	1960	2.60	1.21	200	1823
	1780	1960	4.67	1.21	200	1805
	1890	2100	2.59	1.22	70	1987
	1910	2130	2.39	1.23	50	2034
	1910	2130	2.65	1.23	100	1987
	1940	2170	3.40	1.23	50	2045
	1940	2170	4.08	1.23	80	2006
	2010	2240	3.22	1.23	40	2127
	2040	2280	2.35	1.23	20	2218
	2110	2370	2.17	1.24	15	2315
	2140	2410	3.18	1.25	10	2352
	2220	2500	2.04	1.26	10	2454
	2260	2550	1.73	1.26	6	2523
	2300	2600	2.19	1.26	6	2564
	2300	2600	2.67	1.26	6	2557

calculate temperature of the system from Eq. (5). According to the empirical expression of Millikan and White<sup>7)</sup> (which is not correct theoretically but very useful) where only translation-to-vibration energy conversion was assumed,  $\tau_v$  of the present system is expressed as follows.

$$(P\tau_v)^{-1} = \phi_{N_2}(P\tau_{N_2-N_2})^{-1} + \phi_{NH_3}(P\tau_{N_2-NH_3})^{-1} + \phi_{O_2}(P\tau_{N_2-O_2})^{-1} \quad (6)$$

Here, relaxation times with two subscripts refer to relaxation of the first species when it is present at high dilution in the second-named gas at a total pressure of  $P$  atm, and  $\phi_s$  are mole fractions of components. Although  $\tau_{N_2-O_2}$  is not known, this can be estimated by using an empirical formula of Millikan and White<sup>7)</sup> and was found to be comparable to  $\tau_{N_2-N_2}$ . Since  $\phi_{N_2} \gg \phi_{O_2}$  in the

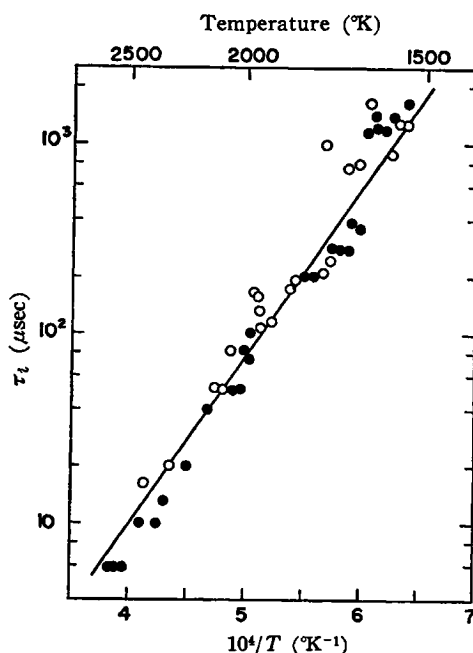


Fig. 4. Arrhenius plot for  $\tau_i$ .

Marks  $\circ$  and  $\bullet$  refer to mixtures XII and XIII respectively and a solid line was calculated from Eqs. (2).

present experimental conditions, the third term in Eq. (6) can be neglected. Therefore, Eq. (6) is expressed as follows.

$$(P\tau_v)^{-1} = \phi_{N_2}(P\tau_{N_2-N_2})^{-1} + \phi_{NH_3}(P\tau_{N_2-NH_3})^{-1} \quad (7)$$

Here,  $\tau_{N_2-N_2}$  is given by Eq. (3), but no information about  $\tau_{N_2-NH_3}$  is available. How-

7) R. C. Millikan and D. R. White, *J. Chem. Phys.*, **39**, 3209 (1963).

ever, recently, White<sup>8)</sup> found that  $\tau_{N_2-He}$ ,  $\tau_{N_2-C_2H_2}$ , and  $\tau_{N_2-CH_4}$  are approximately double, equal to, and 60% of  $\tau_{N_2-H_2}$  in the range of 1600 to 2500°K. Since vibrational frequencies of  $NH_3$  are not close to those of  $N_2$ , much more rapid vibration-to-vibration exchange between  $N_2$  and  $NH_3$  compared with that between  $N_2$  and  $C_2H_2$  or  $CH_4$  is not expected and  $\tau_{N_2-NH_3}$  may be comparable to  $\tau_{N_2-C_2H_2}$  or  $\tau_{N_2-CH_4}$ , that is, to  $\tau_{N_2-H_2}$ . Therefore, as a rather reasonable approximation, let us assume

$$\tau_{N_2-NH_3} \doteq \tau_{N_2-H_2} \quad (8)$$

By using an expression for  $\tau_{N_2-H_2}$  given by White,<sup>9)</sup>  $\tau_{N_2-NH_3}$  is expressed as follows.

$$\log P\tau_{N_2-NH_3} \doteq 35.0(T^{-1/8} - 0.0176) - 8.00 \quad (9)$$

From Eqs. (3), (5), (7), and (9), temperature of the present system can be calculated with a computer by using known values of  $T_a$ ,  $T_b$ ,  $P$ ,  $C_p/C_p'$  and  $\tau_i$  as shown in Table 2,

8) D. R. White, *ibid.*, **48**, 525 (1968).

9) D. R. White, *ibid.*, **46**, 2016 (1967).

where reflected shock pressure  $P$  is an average of those for (a) and (b) since difference between them is less than 0.5% at maximum. Also, calculated values of the temperature  $T$  are shown in the table. Thus, in Fig. 4, values of  $\tau_i$  is plotted against newly obtained values of  $T$ . Here, excellent agreement between both polts for  $NH_3-O_2-N_2$  and  $NH_3-O_2-Ar$  is observed. This agreement suggests that  $\tau_i$  for the  $NH_3-O_2-N_2$  is the same as that for  $NH_3-O_2-Ar$  and possibility of coupling of vibrational relaxation and oxidation reaction is small. However, we cannot say that it is conclusive unless  $\tau_{N_2-NH_3} \doteq \tau_{N_2-H_2}$  is proved. It is a very challenging problem to measure vibrational relaxation times for  $N_2$  dilute in  $NH_3$  and to obtain more detailed informations about kinetics of  $NH_3-O_2-N_2$  system.

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